



Typical Textures, part 1: Thermomechanical Processing (TMP) of Metals

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27-750

Texture, Microstructure & Anisotropy

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Objectives

- Introduce you to experimentally observed textures in a wide range of materials.
- Develop a taxonomy of textures based on deformation type.
- Prepare you for relating observed textures to theoretical (numerical) models of texture development, especially the *Taylor* model.
- See chapter 5 in Kocks, Tomé & Wenk.
- Some slides courtesy of Prof. P. Kalu (FAMU)

Taxonomy

- Deformation history more significant than alloy.
- Crystal structure determines texture through slip (and twinning) characteristics.
- Alloy (and temperature) can affect textures through planarity of slip.
- Annealing (recrystallization) sometimes produces a drastic change in texture.

Why does deformation result in texture development?

- Qualitative discussion:
- Deformation means that a body changes its shape, which is quantified by the plastic strain, ε_p .
- Plastic strain is accommodated in crystalline materials by dislocation motion, or by re-alignment of long chain molecules in polymers.

Dislocation glide \Rightarrow *grain reorientation*

- Dislocation motion at low (homologous) temperatures occurs by glide of loops on crystallographic planes in crystallographic directions: *restricted glide*.
- Restricted glide throughout the volume is equivalent to uniform shear.
- In general, shear requires lattice rotation in order to maintain grain alignment: *compatibility*

Re-orientation → Preferred orientation

- Reorientations experienced by grains depend on the type of strain (compression versus rolling, e.g.) and the type of slip (e.g. $\{111\}\langle 110\rangle$ in fcc).
- In general, some orientations are unstable ($f(g)$ decreases) and some are stable ($f(g)$ increases) with respect to the deformation imposed, hence *texture development*.

The Taylor model

- The *Taylor* model has one basic assumption: the change in shape (micro-strain) of each grain is identical to the body's change in shape (macro-strain).
- Named for G.I. Taylor, English physicist, mid-20th century; first to provide a quantitative explanation of texture development.

Single slip models ineffective

- Elementary approach to single crystal deformation emphasizes slip on a single deformation system.
- Polycrystal texture development requires *multiple slip systems* (5 or more, as dictated by von Mises).
- *Cannot use simple rules*, e.g. alignment of slip plane with compression plane!

Deformation systems (typical)

- Fcc metals
(low temperature):
 $\{111\}\langle 110\rangle$
- Bcc metals:
 $\{110\}\langle 111\rangle$,
 $\{112\}\langle 111\rangle$,
 $\{123\}\langle 111\rangle$,
pencil glide
- Hexagonal metals:
 $\{1010\}\langle 1210\rangle$;
 $\{0001\}\langle 1210\rangle$;
 $\{1012\}\langle 1011\rangle_{\text{twin}}$;
 $\{1011\}\langle 1123\rangle$;
 $\{2112\}\langle 2113\rangle_{\text{twin}}$.

Deformation systems (typical)

Material Class	Primary System	Secondary Systems
Face-centered cubic metals	$\{111\} \langle 1\bar{1}0 \rangle$	
Body-centered cubic metals	$\{110\} \langle 111 \rangle$	$\{123\} \langle 1\bar{1}\bar{1} \rangle$ $\{112\} \langle 11\bar{1} \rangle$
Hexagonal close-packed metals ($c/a > 1.633$) (e.g. Be, Cd, Zn and Mg)	$\{0001\} \langle 11\bar{2}0 \rangle$	$\{11\bar{2}2\} \langle 11\bar{2}3 \rangle$ $\{10\bar{1}1\} \langle 11\bar{2}0 \rangle$
Hexagonal close-packed metals ($c/a < 1.633$) (e.g. Zr, Ti and Hf)	$\{10\bar{1}0\} \langle 11\bar{2}0 \rangle$	$\{11\bar{2}2\} \langle 11\bar{2}3 \rangle$ $\{10\bar{1}1\} \langle 11\bar{2}0 \rangle$
Diamond cubic (fcc) (e.g. Si, Ge and diamond)	$\{111\} \langle 1\bar{1}0 \rangle$	
Rock Salt (fcc) (e.g. MgO, LiF, NaCl)	$\{110\} \langle 1\bar{1}0 \rangle$	
CsCl (simple cubic)	$\{110\} \langle 001 \rangle$	
Al ₂ O ₃ (hexagonal)	$\{0001\} \langle 11\bar{2}0 \rangle$	$\{11\bar{2}0\} \langle 1\bar{1}01 \rangle$ $\{1\bar{1}02\} \langle 1\bar{1}01 \rangle$
BeO (hexagonal)	$\{0001\} \langle 11\bar{2}0 \rangle$	$\{10\bar{1}0\} \langle 11\bar{2}0 \rangle$ $\{10\bar{1}0\} \langle 0001 \rangle$

In deformed materials, texture or preferred orientation exists due to the anisotropy of slip. While slip in bcc metals generally occurs in the $\langle 111 \rangle$ type direction, it may be restricted to $\{110\}$ planes or it may involve other planes

(T. H. Courtney, *Mechanical Behavior of Materials*, McGraw-Hill, New York, 1990.)

Strain Measures

- Strain commonly defined as a scalar measure of (plastic, irreversible) deformation: logarithmic strain:=

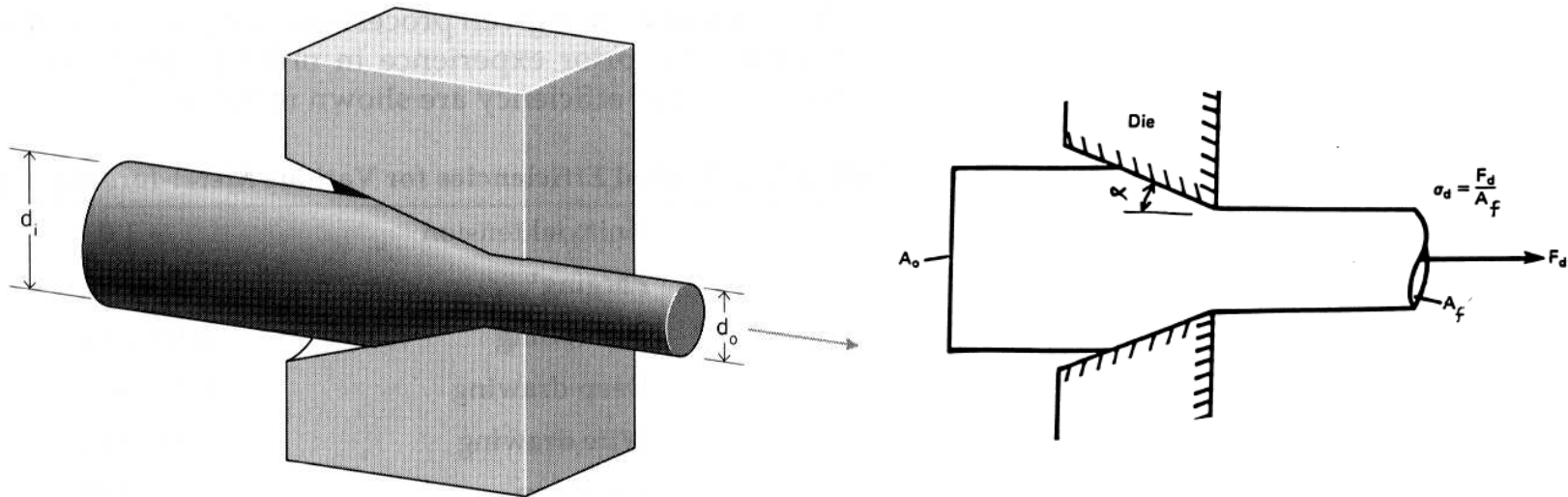
$$\varepsilon = \ln \{l_{\text{new}}/l_{\text{old}}\}$$
- Rolling strain: typical: reduction in thickness:= $r = 100\% \times h_{\text{new}}/h_{\text{old}}$
 better (!) = *von Mises equivalent strain*

$$\varepsilon_{\text{vM}} = 2/\sqrt{3} \ln \{l_{\text{old}}/l_{\text{new}}\}$$

Deformation Modes: sample symmetry

- Tension, Wire Drawing, Extrusion C_{∞}
- Compression, Upsetting C_{∞}
- Torsion, Shear 2
- Plane Strain Compression, Rolling mmm
- Deformation modes of uniaxial type generate fiber textures
- Shear gives monoclinic symmetry
- Plane strain gives orthorhombic symmetry

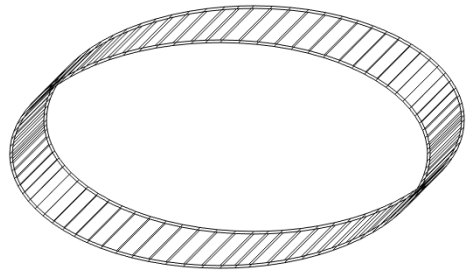
Axisymmetric deformation: Extrusion, Drawing



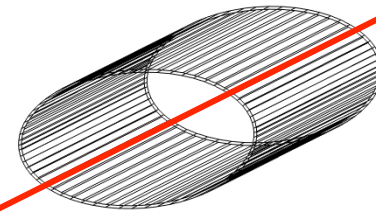
$$\varepsilon = \begin{pmatrix} +\Delta & 0 & 0 \\ 0 & -0.5\Delta & 0 \\ 0 & 0 & -0.5\Delta \end{pmatrix}$$

Uniaxial Strain

$$d\varepsilon = \begin{pmatrix} +\Delta & 0 & 0 \\ 0 & -\Delta/2 & 0 \\ 0 & 0 & -\Delta/2 \end{pmatrix}$$

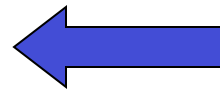
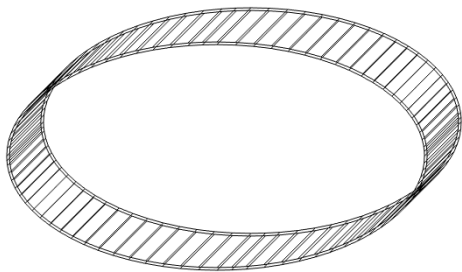
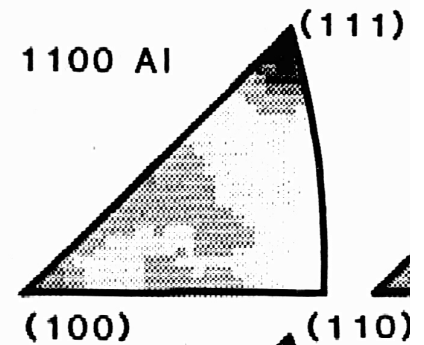


tension

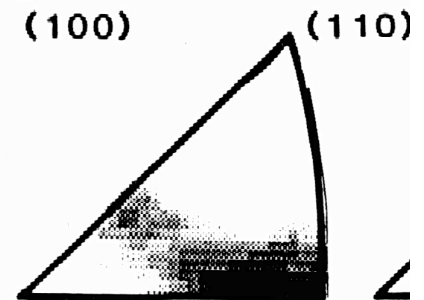
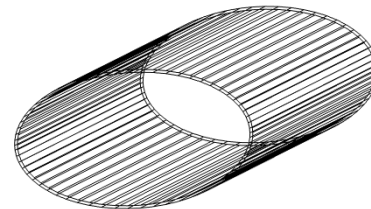


C_{∞}

Inverse
Pole
Figures
(FCC)



compression



$$d\varepsilon = \begin{pmatrix} -\Delta & 0 & 0 \\ 0 & +\Delta/2 & 0 \\ 0 & 0 & +\Delta/2 \end{pmatrix}$$

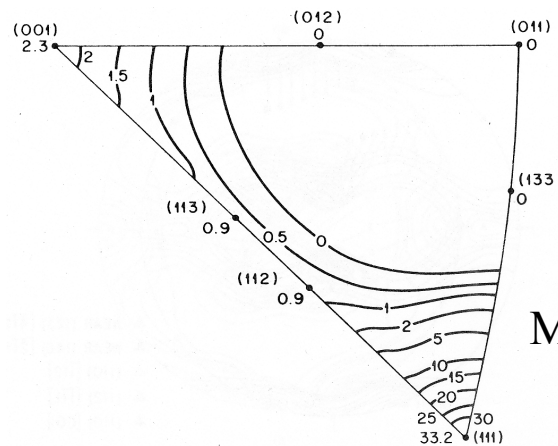
Uniaxial Modes - C_{∞}

<u>Deformation mode/</u>	<u>fcc/</u>	<u>bcc/</u>	<u>hcp (Ti)</u>
Wire drawing, Round extrusion.	<111> & <100>	<110>	<10-10>
Upsetting, Uniaxial compression.	<110>	<111> &<100>	<0001>

Note exchange of types between *fcc* & *bcc*

Axisymmetric deformation

- In fcc metals, axisymmetric deformation (e.g. wire drawing) produces fiber texture: $\langle 111 \rangle + \langle 100 \rangle$ duplex, parallel to the wire.

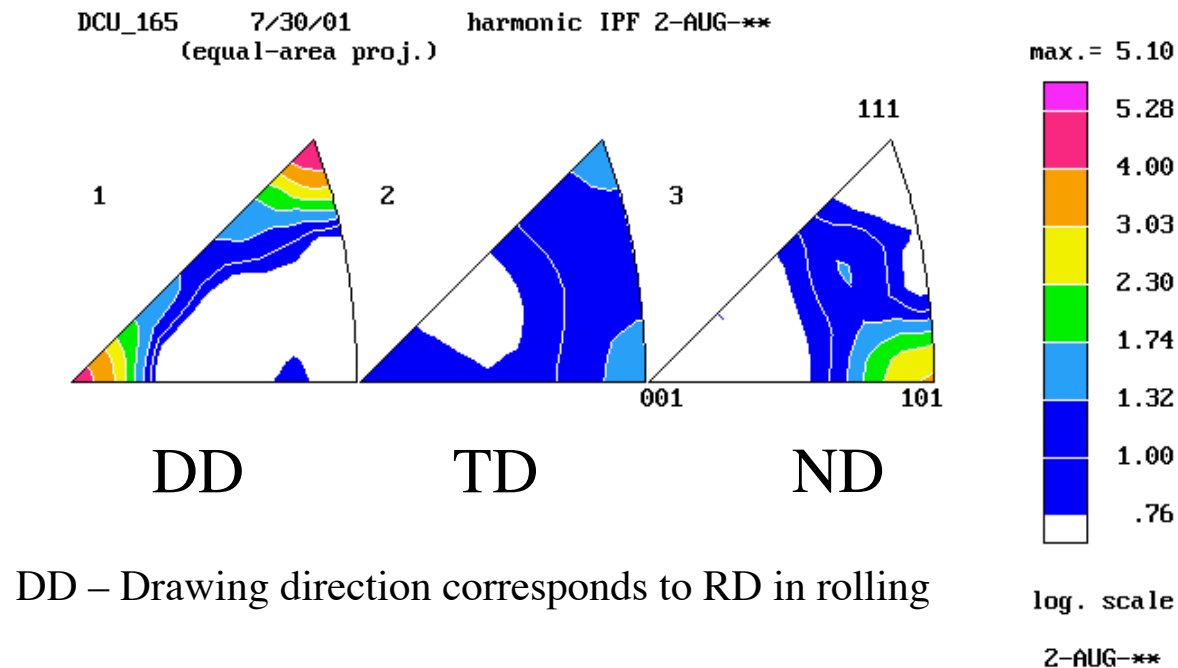


McHargue et al., 1959

Schmid and Wassermann (1963): 60% $\langle 111 \rangle + 40\%$ $\langle 100 \rangle$ } Electrolytic
 Ahlborn and Wassermann (1963): 66% $\langle 111 \rangle + 34\%$ $\langle 100 \rangle$ } Copper

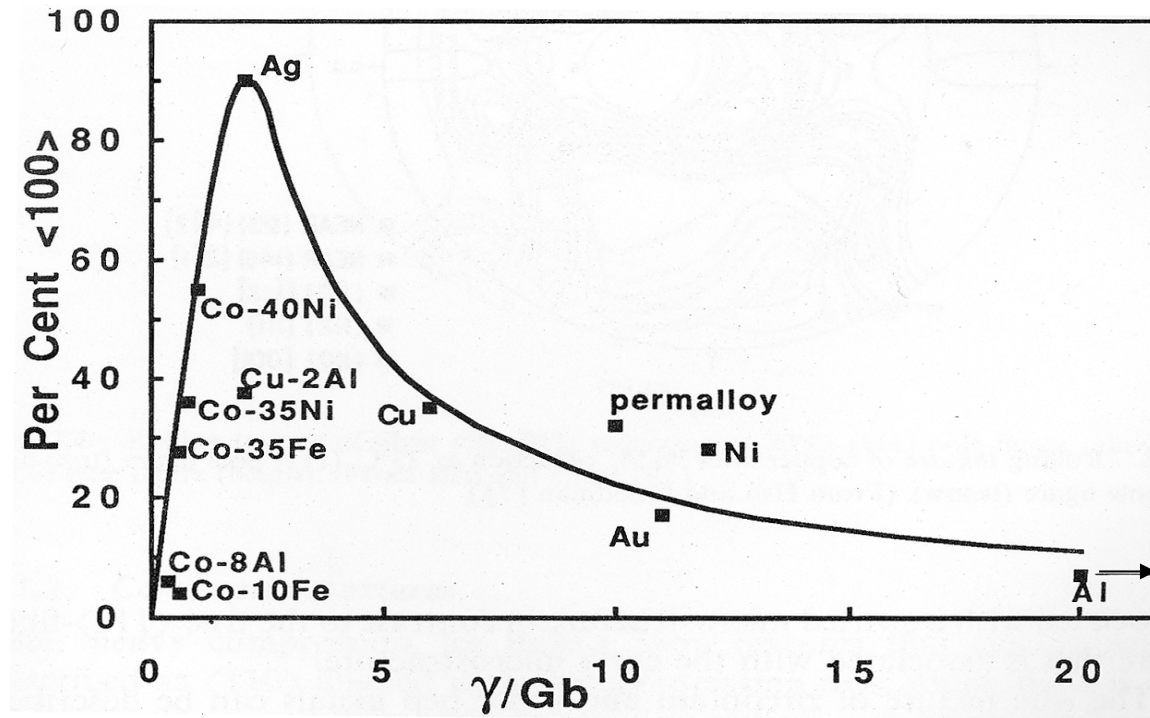
Axisymmetric deformation

- Axisymmetric deformation ~ higher order symmetry, C_{∞}
- Texture can be represented by an *inverse pole figure* (IPF).
- In IPF, contour lines show the frequency with which the various directions, $\langle uvw \rangle$, in the crystal coincide with the specimen axis under consideration

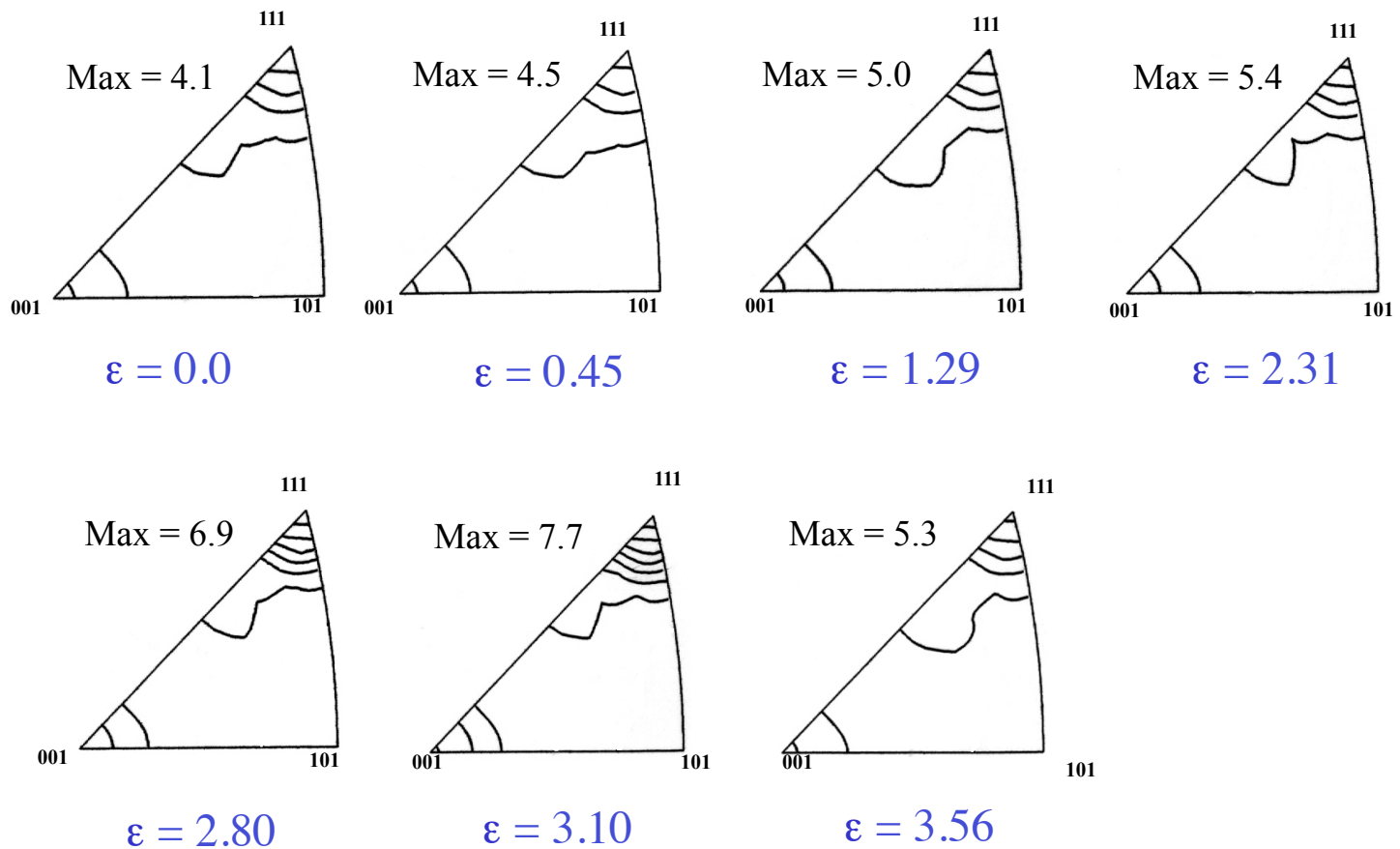


Axisymmetric deformation

- The relative proportions of the two components are determined by the stacking fault energy [English et al., 1965] and vary in a complex manner.

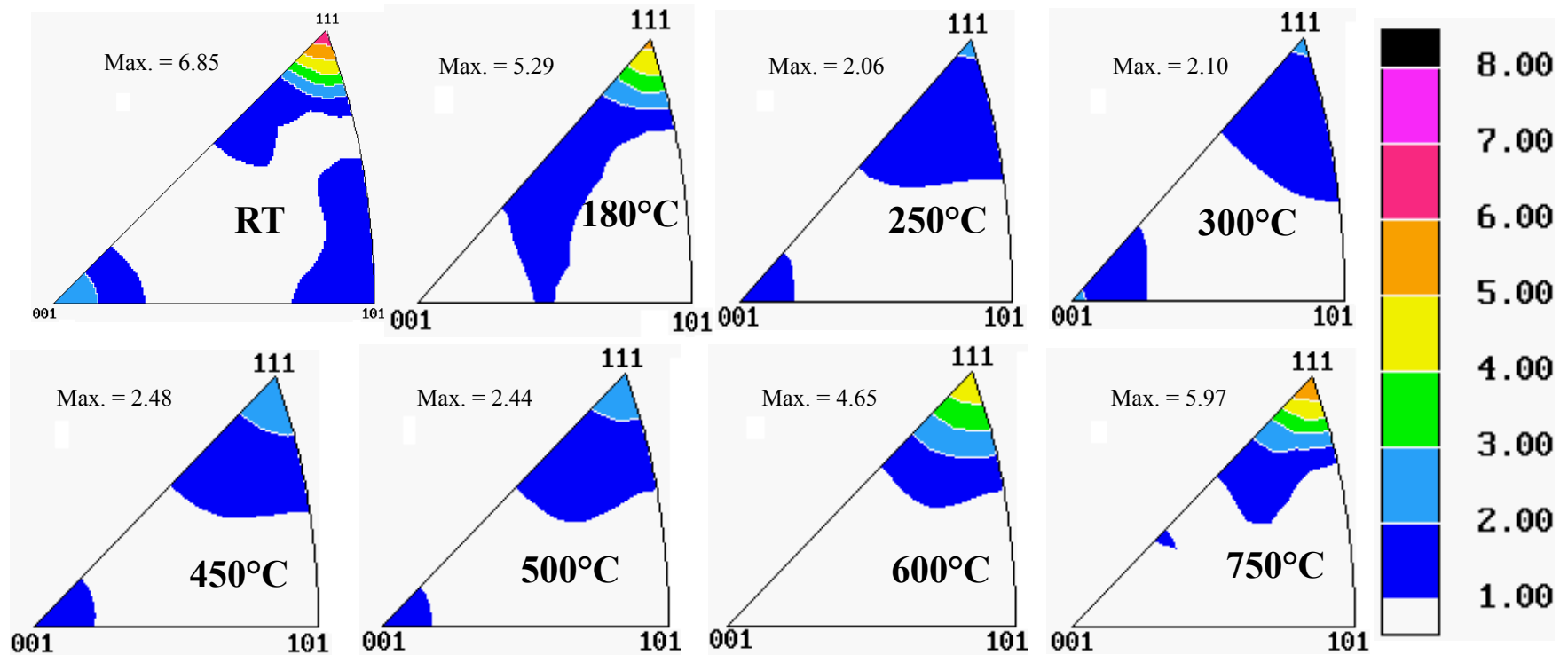


Effect of deformation strain



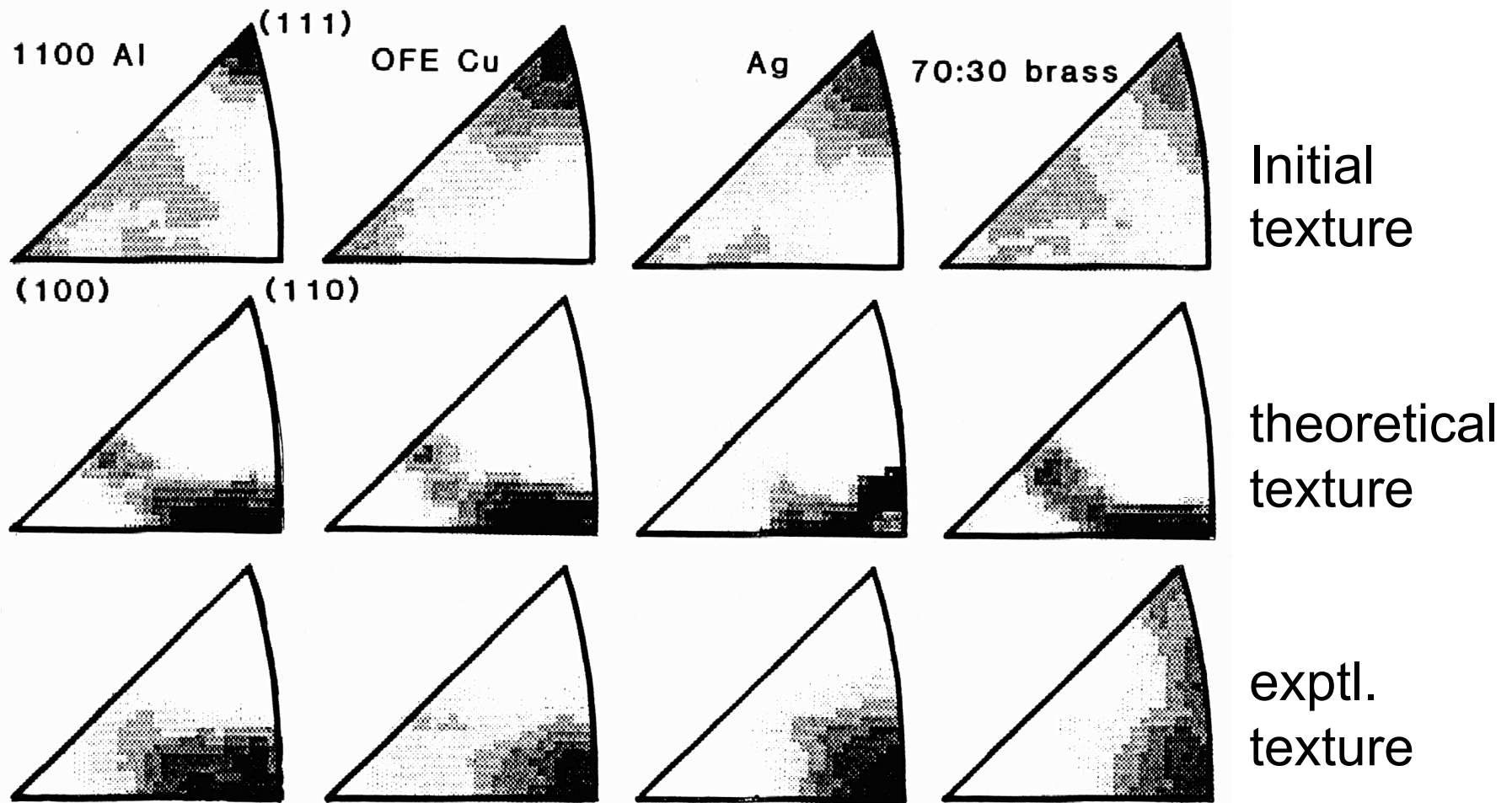
X-ray IPFs showing the effect of strain on the texture of OFHC copper wire

Effect of Temperature



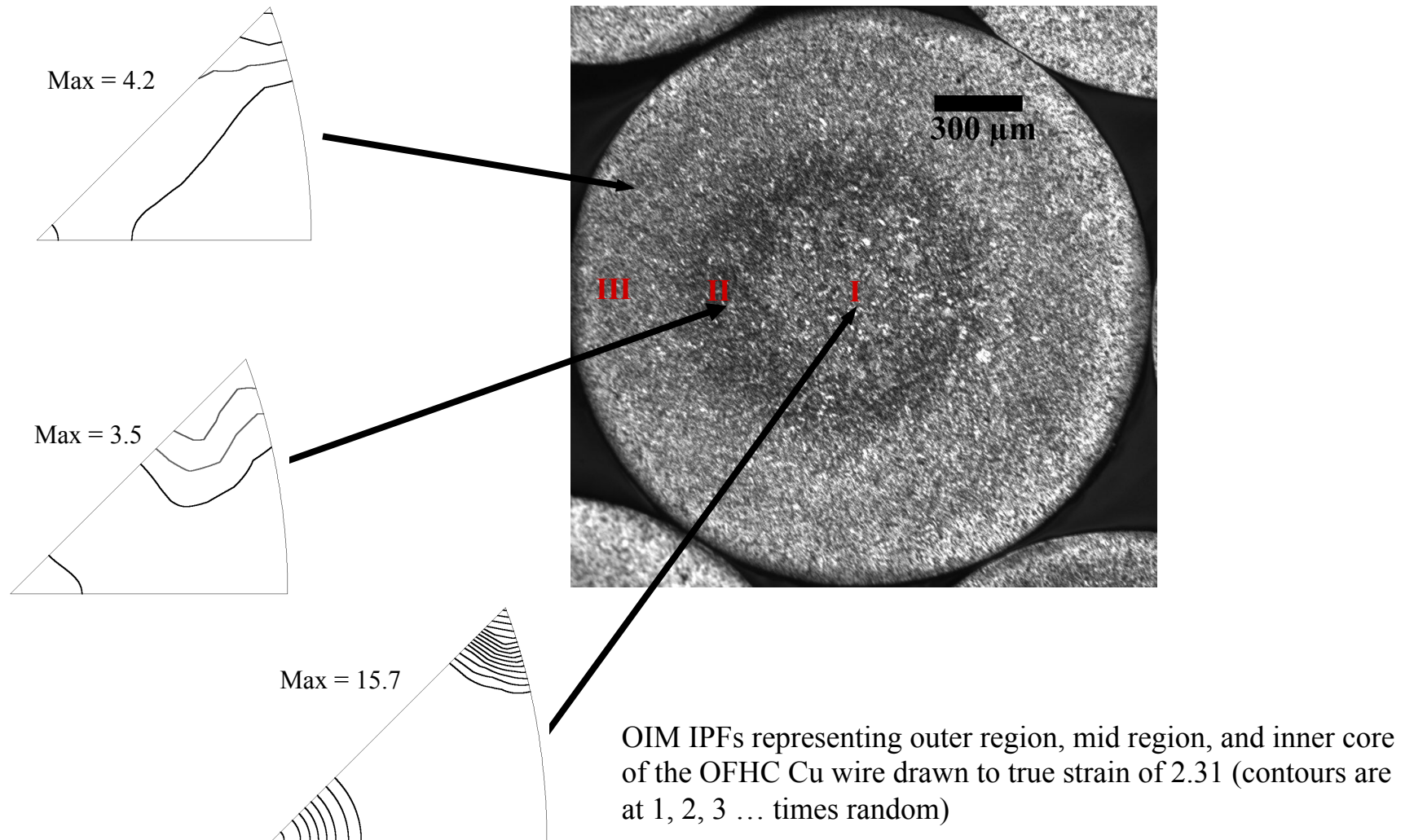
X-ray IPFs showing the effect of annealing temperature on the texture of OFHC copper wire, initially drawn to true strain of 2.31

Uniaxial Compression: fcc

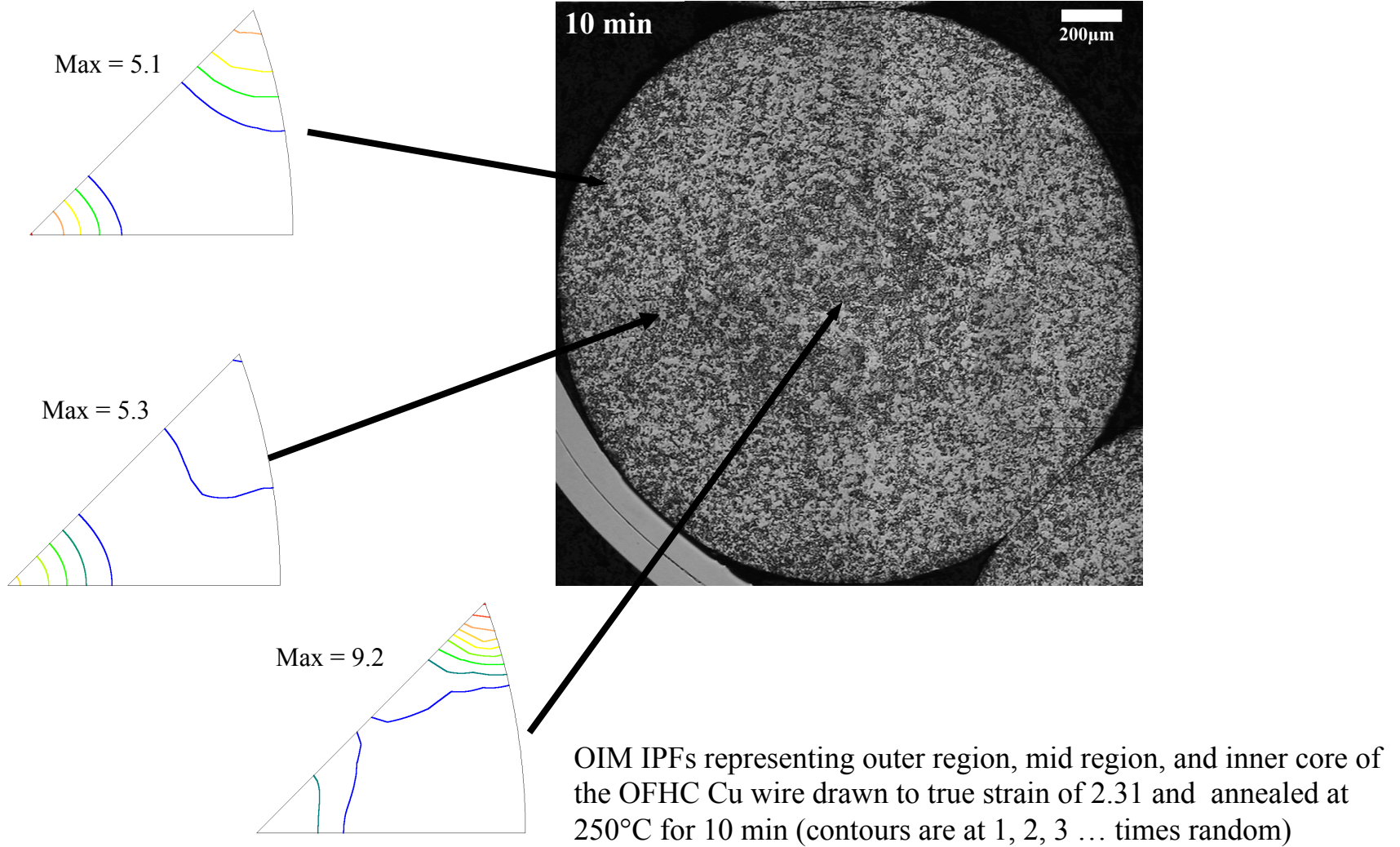


[Kocks Ch. 5: Inverse Pole Figures]

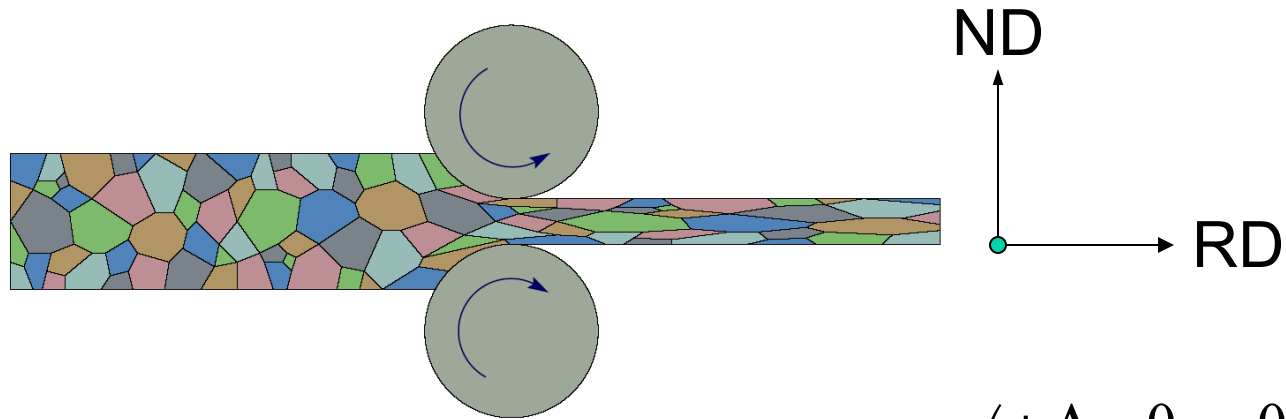
Texture inhomogeneity in Drawn Wires



Texture inhomogeneity in Drawn Wires



Rolling = Plane Strain

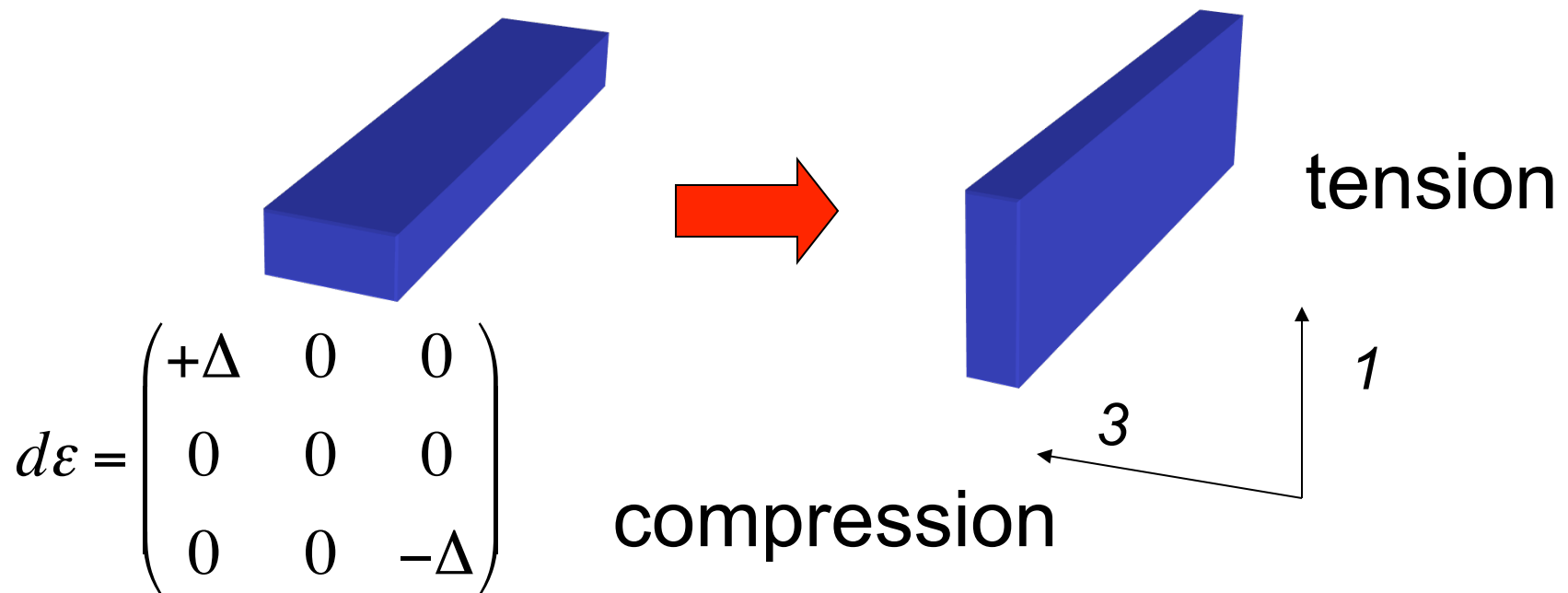


$$\varepsilon = \begin{pmatrix} +\Delta & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & -\Delta \end{pmatrix}$$

Rolling ~ plane strain deformation means extension or compression in a pair of directions with zero strain in the third direction: a *multiaxial strain*.

Plane strain (rolling)

Plane strain means extension/compression in a pair of directions with zero strain in the third direction: a *multiaxial strain*.



Typical rolling texture in FCC Materials

Type	Component	$\{hkl\}\langle uvw \rangle$	Euler Angles (Bunge)		
			φ_1	θ	φ_2
Deformation	Bs	$\{011\}\langle 211 \rangle$	35	45	0
	S	$\{123\}\langle 634 \rangle$	55	35	65
	Cu	$\{112\}\langle 111 \rangle$	90	30	45
	Shear ₁	$\{001\}\langle 110 \rangle$	0	0	45
	Shear ₂	$\{111\}\langle 110 \rangle$	0	55	45
	Shear ₃	$\{112\}\langle 110 \rangle$	0	35	45
Recrystallization	Goss	$\{011\}\langle 001 \rangle$	0	45	0
	Cube	$\{001\}\langle 100 \rangle$	0	0	0
	RC _{RD1}	$\{013\}\langle 100 \rangle$	0	20	0
	RC _{RD2}	$\{023\}\langle 100 \rangle$	0	35	0
	RC _{ND1}	$\{001\}\langle 310 \rangle$	20	0	0
	RC _{ND2}	$\{001\}\langle 320 \rangle$	35	0	0
	P	$\{011\}\langle 122 \rangle$	70	45	0
	Q	$\{013\}\langle 231 \rangle$	55	20	0
	R	$\{124\}\langle 211 \rangle$	55	75	25

fcc/	bcc/	hcp (Ti)
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Shear:

A: {111} <uvw>

E: {110} <001>

??

B: {hkl} <110>

D: {112} <110>

C: {001} <110>

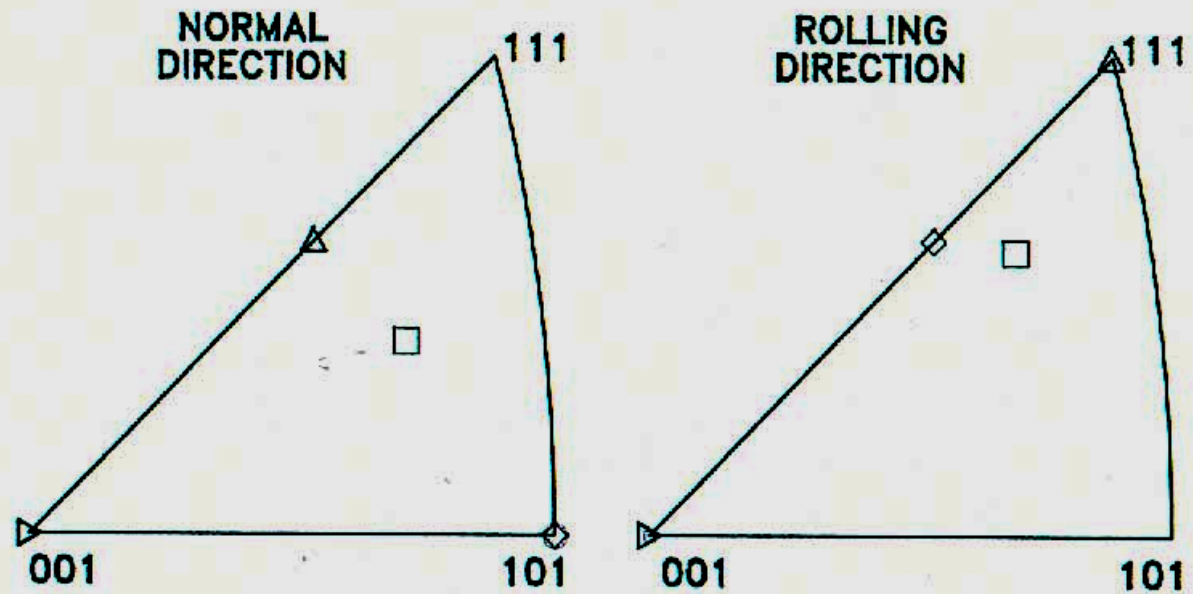
Rolling: Partial Fibers:

beta, alpha

gamma, alpha

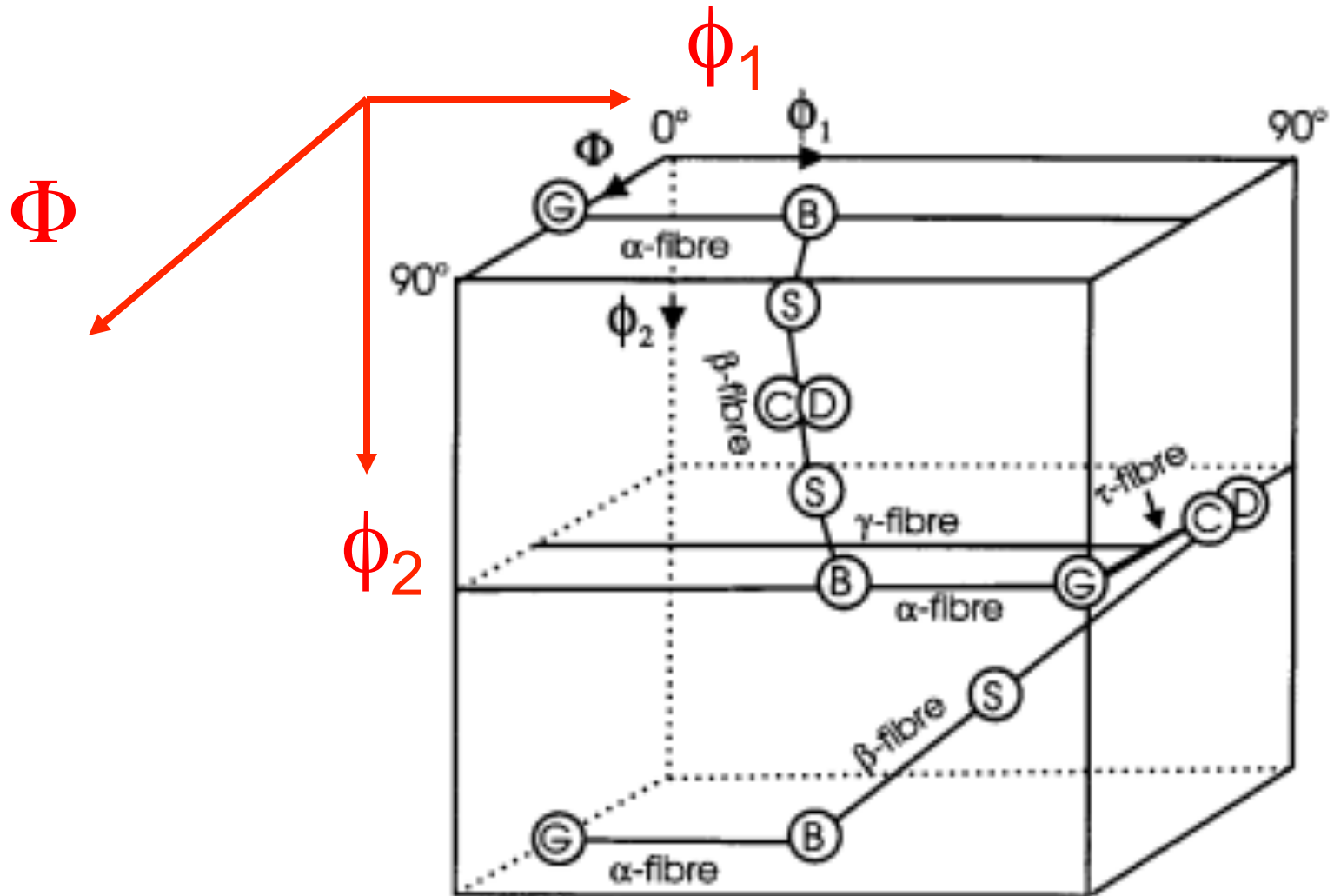
{0001}

INVERSE POLE FIGURES IDEAL ORIENTATIONS



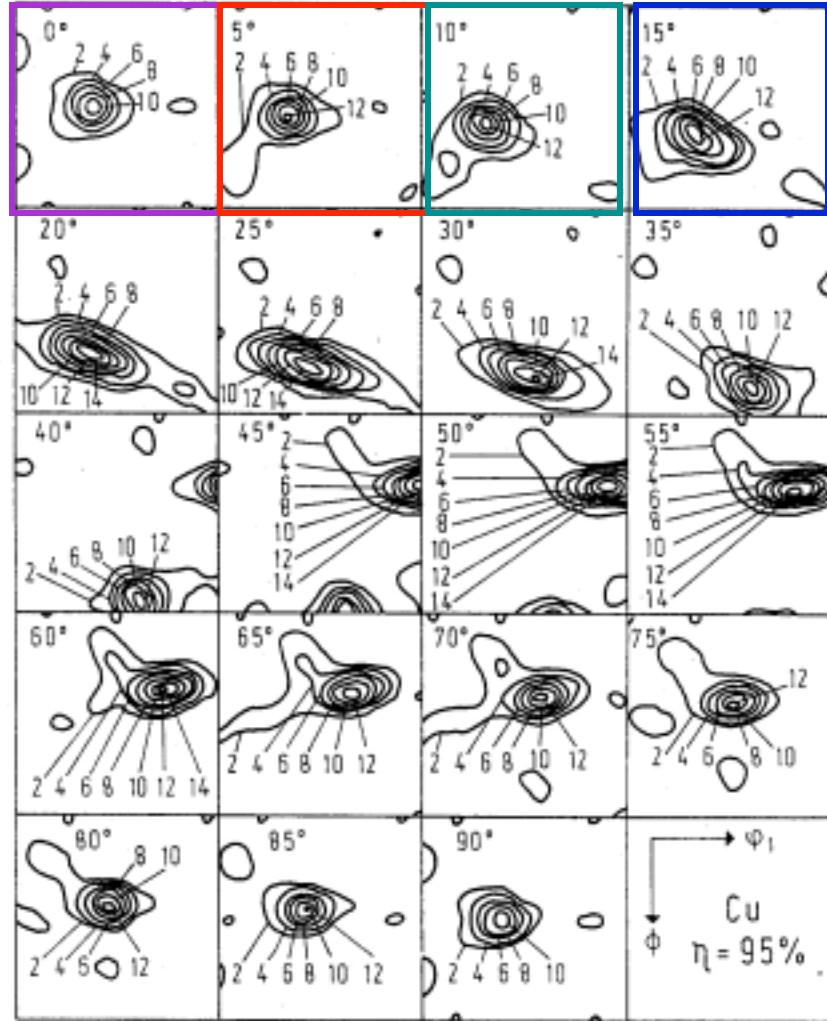
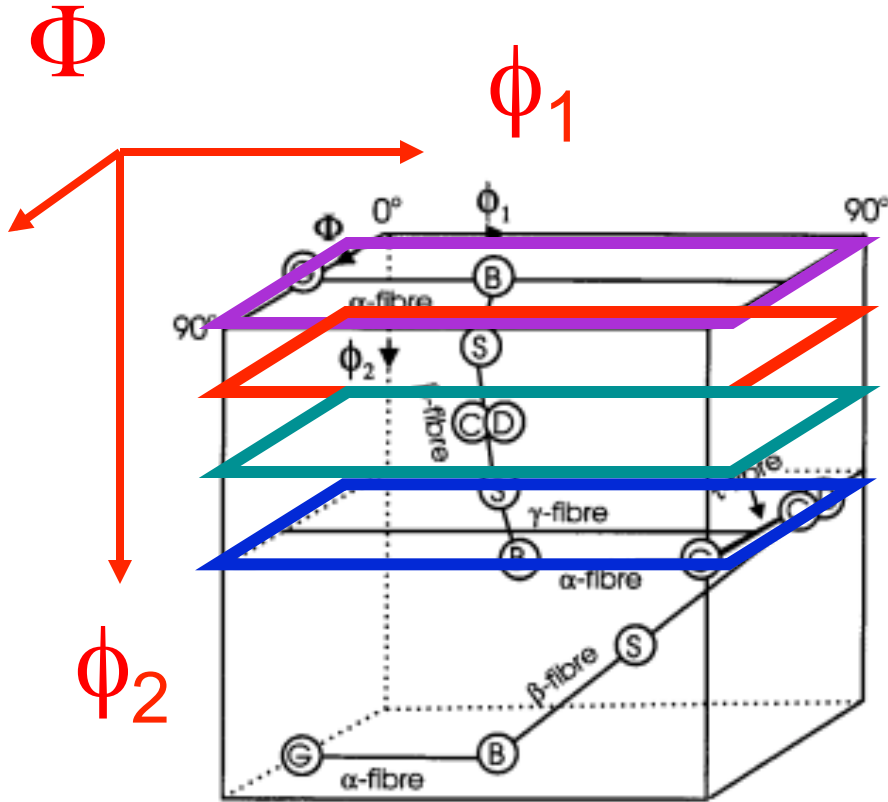
- △ COPPER $\{112\}\langle 11-1 \rangle$
- ◇ BRASS $\{110\}\langle 1-12 \rangle$
- S $\{123\}\langle 63-4 \rangle$
- ▷ CUBE $\{100\}\langle 001 \rangle$
- GOSS $\{110\}\langle 001 \rangle$

Cartesian Euler Space



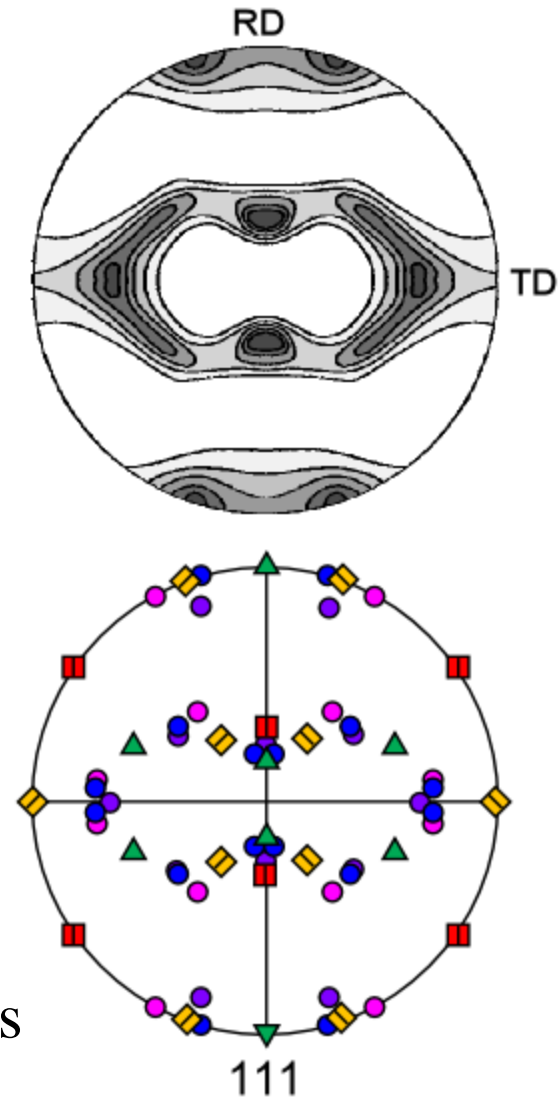
Sections

$\phi_2 = 0^\circ$ $\phi_2 = 5^\circ$ $\phi_2 = 10^\circ$ $\phi_2 = 15^\circ$



PF Representation

Name	Indices	Bunge ($\varphi_1, \Phi, \varphi_2$)
▲ copper	{112}<11 $\bar{1}$ >	90°, 35°, 45°
● S1	{124}<21 $\bar{1}$ >	59°, 29°, 63°
● S2	{123}<41 $\bar{2}$ >	47°, 37°, 63°
● S3*	{123}<63 $\bar{4}$ >	59°, 37°, 63°
◆ brass	{110}< $\bar{1}$ 12>	35°, 45°, 0°
Taylor	{4 4 11}<11 1 $\bar{1}$ 8>	7°, 71°, 70°
■ Goss	{110}<001>	0°, 45°, 0°



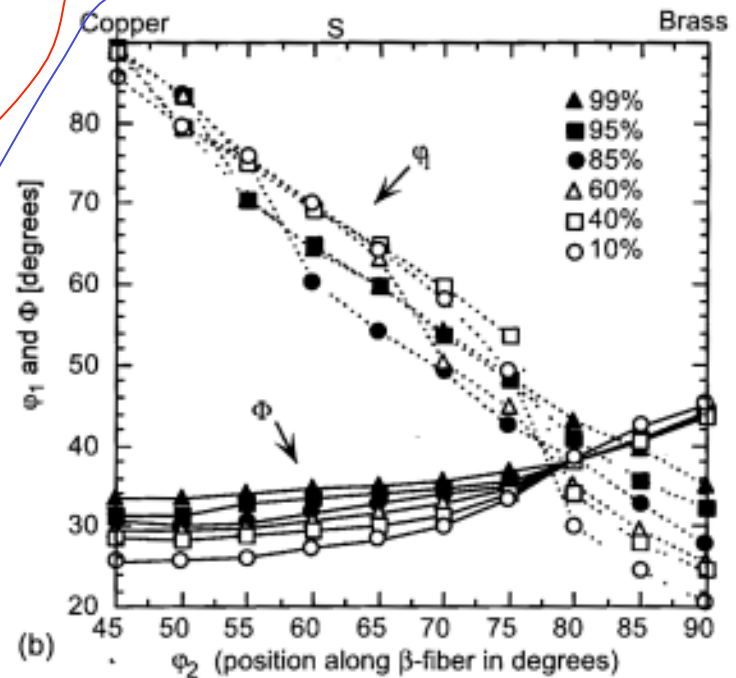
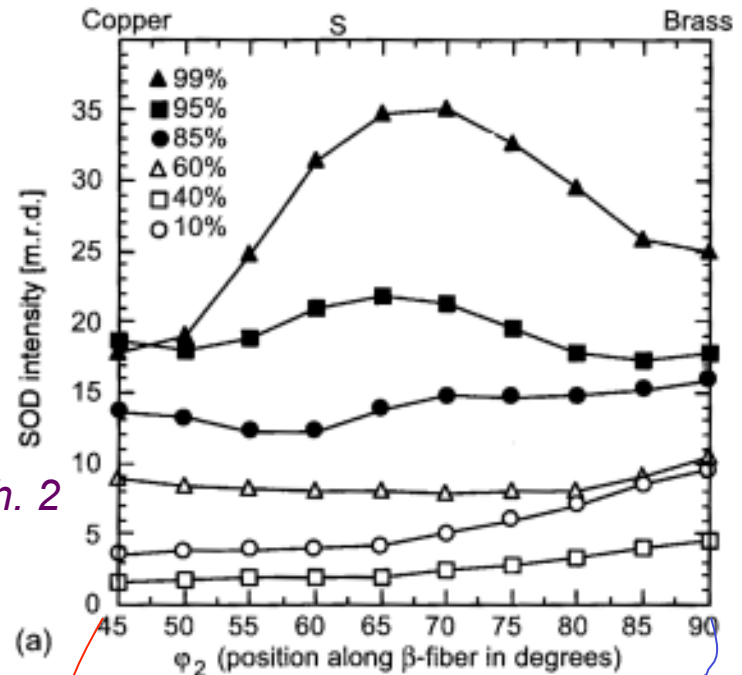
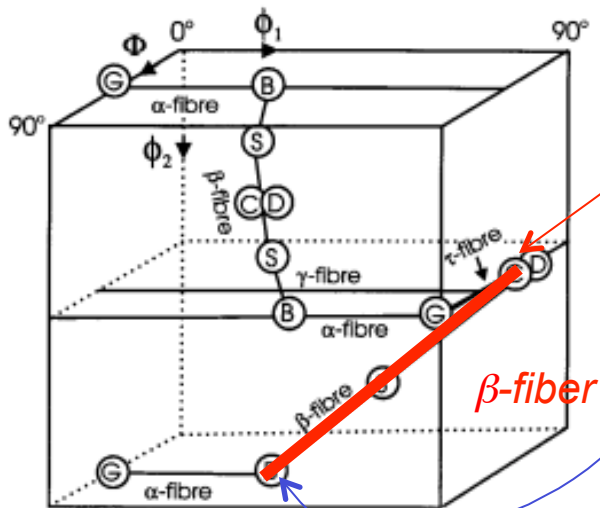
Note how very different components tend to overlap in a pole figure.

Fiber Plots:

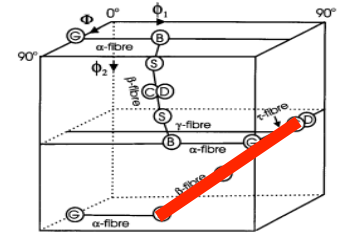
various rolling reductions:
 (a) intensity versus position along the fiber

(b) angular position of intensity maximum versus position along the fiber

Kocks, Ch. 2

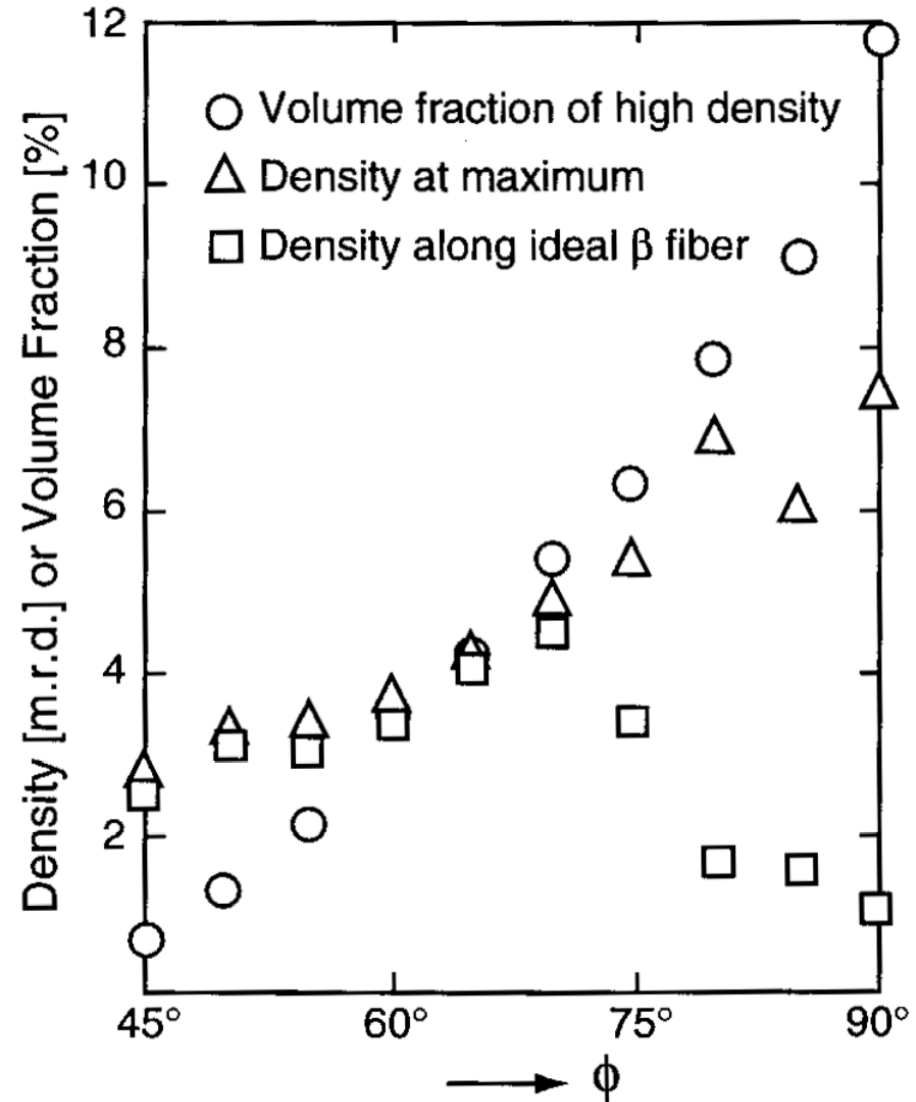


Volume fraction vs. density (intensity)

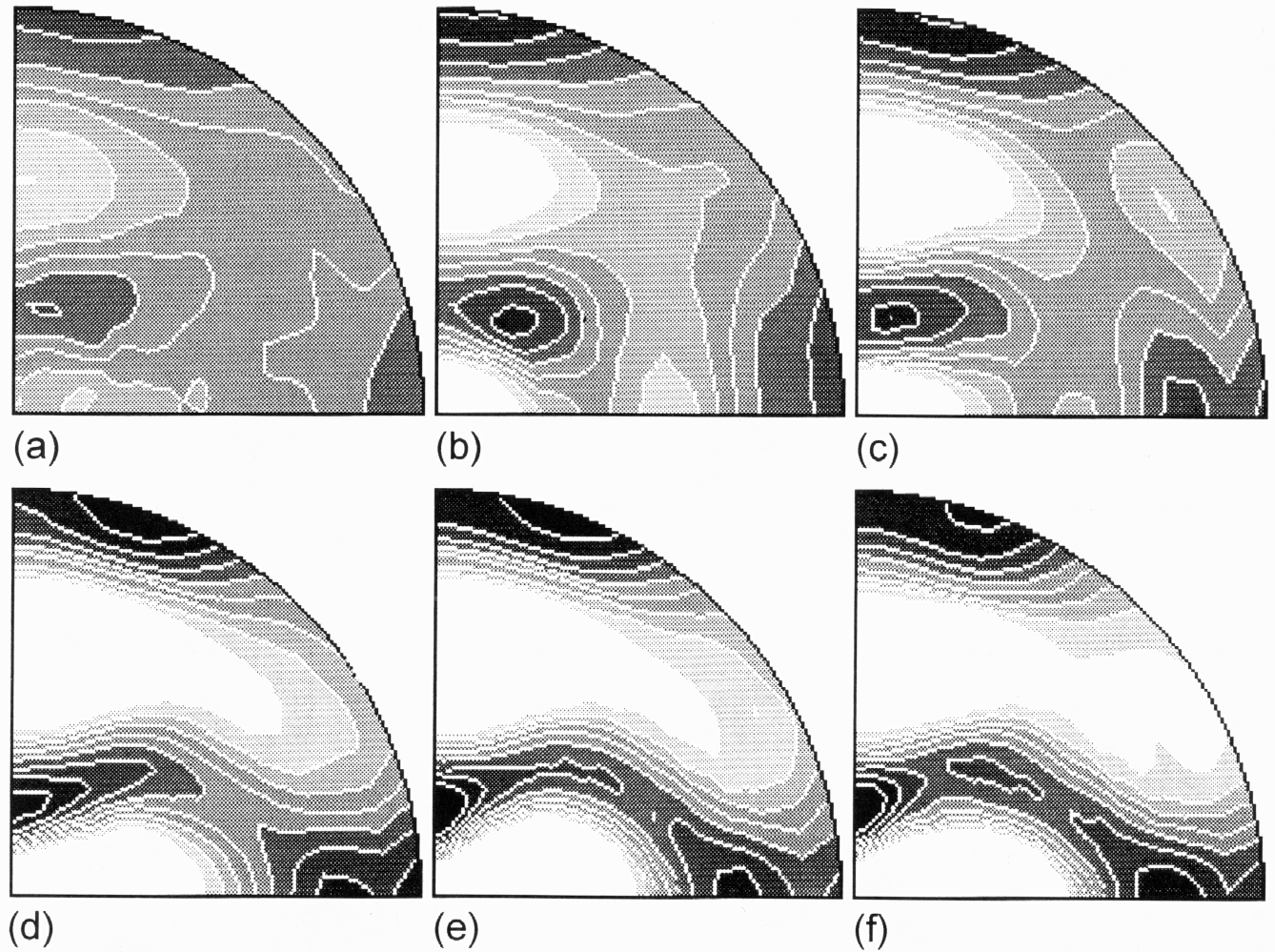


- Volume fraction associated with region around the fiber in a given section.
- V_f increases faster than density with increasing Φ .
- Location of max. density not at nominal location.

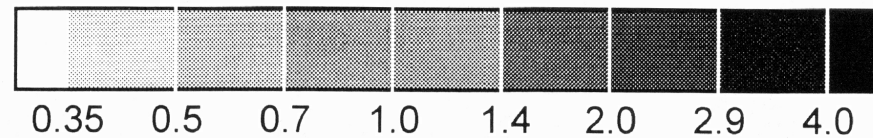
Kocks, Ch. 2



*Rolling
fcc Cu:
Effect of
Strain*

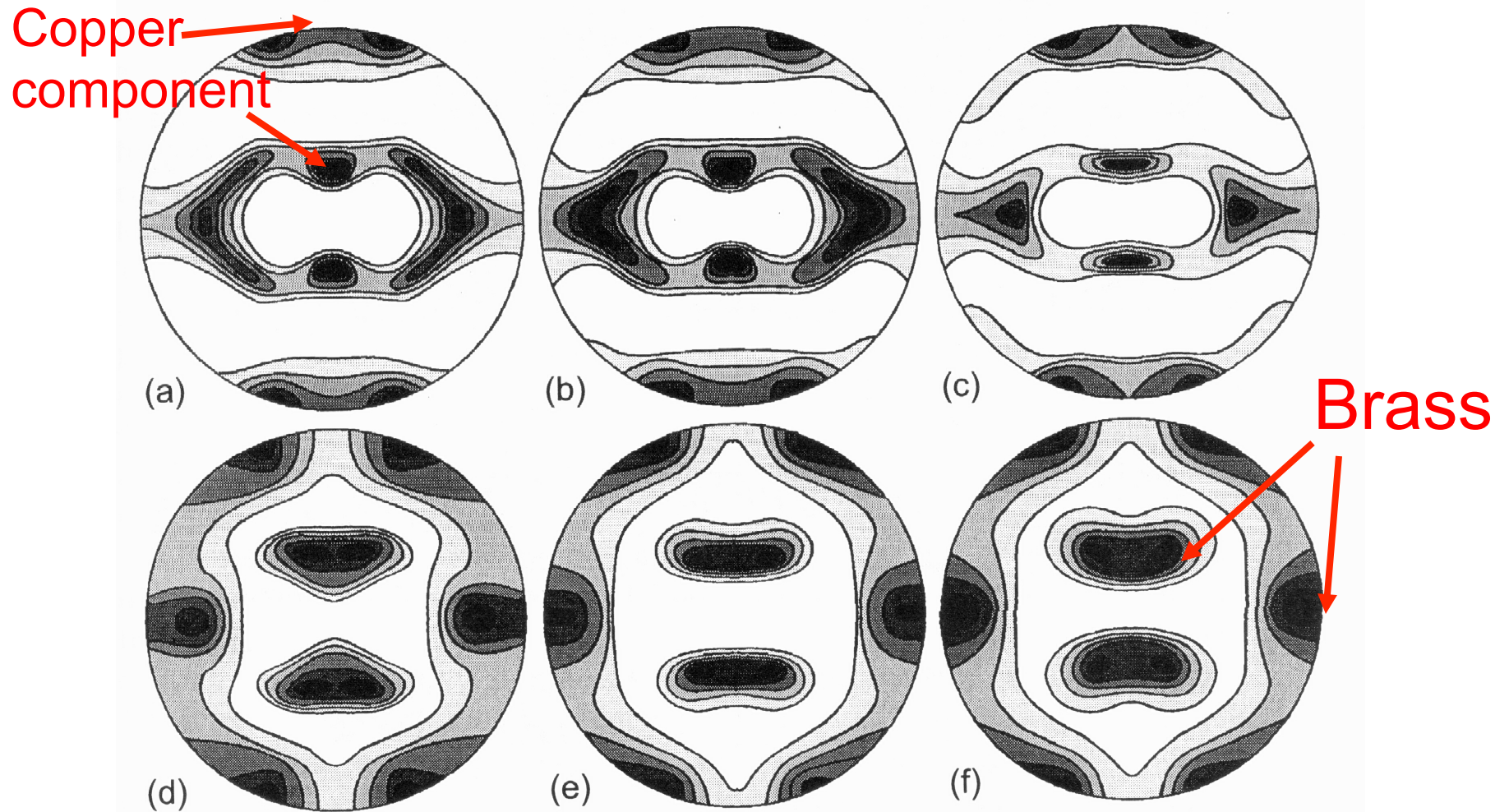


{111} Pole Figures,
RD vertical



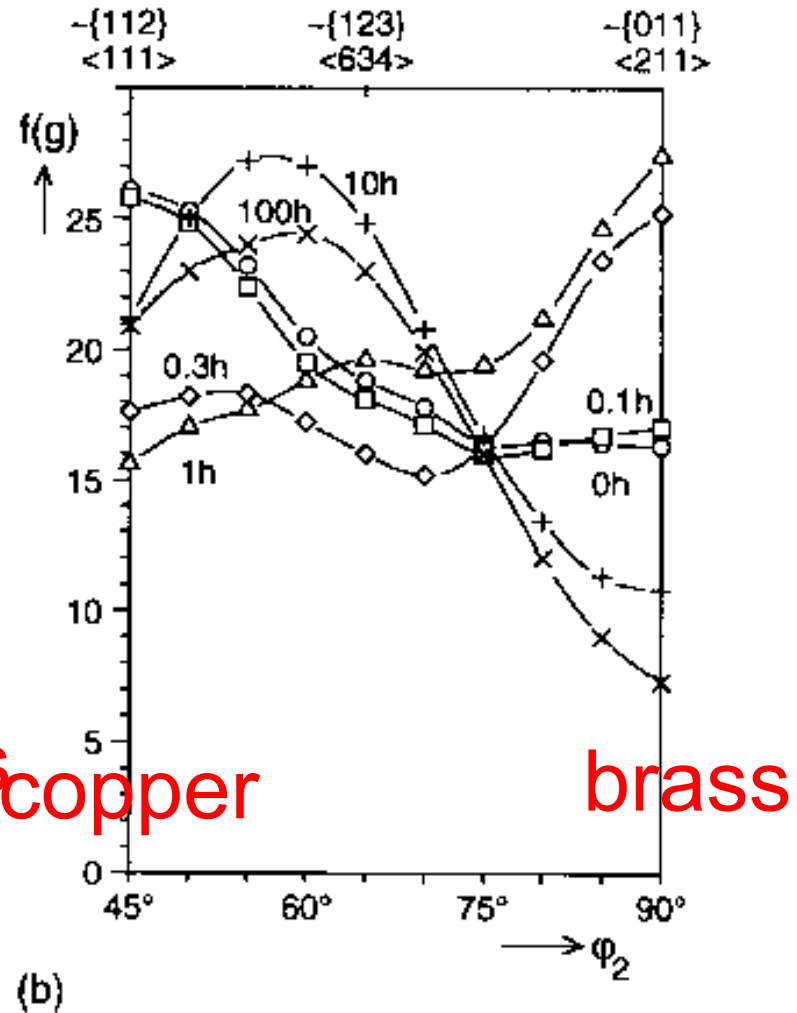
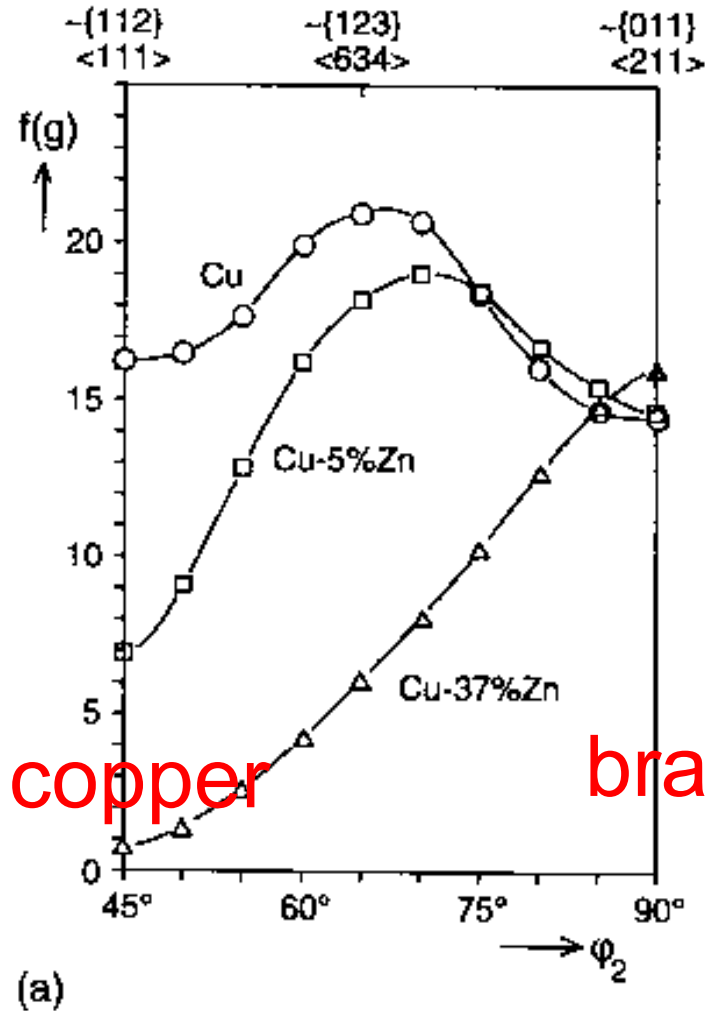
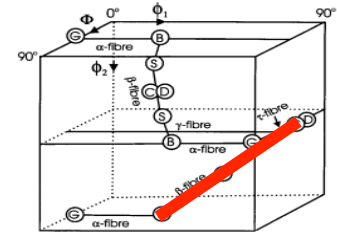
von Mises strains= initial, 0.5, 1.0, 2.0, 2.7, 3.5

Effect of Alloying: Cu-Zn (brass); the texture transition



Zn content: (a) 0%, (b) 2.5%, (c) 5%, (d) 10%, (e) 20% and (f) 30% [Stephens PhD, U Arizona, 1968]

Alloy, Precipitation Effects



Summary: part 1

- Typical textures illustrated for FCC metals as a function of alloy type (stacking fault energy) and deformation character (strain type).
- Pole figures are recognizable for standard deformation histories but orientation distributions provide much more detailed information. Inverse pole figures are also useful, especially for uniaxial textures.
- Measure strain using von Mises equivalent strain.
- Plane strain (rolling) textures concentrate on characteristic lines ("partial fibers") in orientation space.
- Uniaxial textures align certain crystal axes with the deformation axis.

