27-750, A.D. Rollett Due: 16th March, 2016.

Homework 6, Single Slip, and Multiple Slip Crystal Plasticity

- Q1. [30 points] *Single Slip: Calculating Schmid Factors*In a single crystal tensile test on Ni, the orientation of the crystal is given as (18.89, 68.58, 11.31°) in Bunge Euler angles. Assume that an axisymmetric tensile stress is applied along the sample 3 (Z) direction. Note that we apply stress boundary conditions.
- (a) Determine which crystal direction is parallel to the *tensile axis*. Give your answer in the form of (hkl)[uvw] and simplify the numbers to be single digit integers. You should be able to modify the spreadsheet or program that you wrote in earlier homeworks to produce an answer.
- (b) Identify which combination of slip plane and direction is active, and calculate the Schmid factor (to 3 significant figures).

Note: Ni is fcc and can slip on any {111} plane in any <110> direction. You will have to find out which is the most highly stressed slip system, i.e. find the largest Schmid factor. This value of the Schmid factor is what you should use to determine the tensile yield stress because it determines which slip system will be activated first.

(c) Calculate the tensile yield stress (to 3 significant figures) based on a critical resolved shear stress that we will (arbitrarily) set at 100 MPa.

| | | n | - | - | _ | | | | | | I/ | |
|----|----------------------------------|----|----|----|----|-----|-------------|-----------|------------|------------|-------------|-------------------|
| | Α | В | С | D | Е | F | G | H | | J | K | L |
| | | | ٠. | | | | dot | | | Schmid | | |
| 1 | h | k | | u | V | W | product | cos phi | cos lambda | Factor | ABS(Schmid) | |
| 2 | 1 | 1 | 1 | ۲ | 1 | 0 | 0 | 0.843274 | 0.51639778 | 0.43546484 | 0.435464843 | 0.489897949 |
| | | | | | | | | | | | | largest Abs of |
| 3 | -1 | 1 | 1 | 1 | 0 | 1 | 0 | 0.6324555 | | 0.24494897 | 0.244948974 | Schmid |
| 4 | 1 | -1 | 1 | ۲ | 0 | -1 | 0 | -0.210819 | -0.1290994 | 0.02721655 | 0.027216553 | |
| | | | | | | | | | | | | critical resolved |
| | | | | | | | | | | | | yield stress |
| 5 | -1 | -1 | 1 | 1 | 0 | 1 | 0 | -0.421637 | 0.38729833 | -0.1632993 | 0.163299316 | (input) |
| 6 | 1 | 1 | 1 | -1 | 0 | 1 | 0 | 0.843274 | 0.12909944 | 0.10886621 | 0.108866211 | 100 |
| 7 | -1 | 1 | 1 | 0 | -1 | 1 | 0 | 0.6324555 | -0.3872983 | -0.244949 | 0.244948974 | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | observed tensile |
| | | | | | | | | | | | | yield stress = |
| | | | | | | | | | | | | tau_crss/max_S |
| 8 | 1 | -1 | 1 | 1 | 1 | 0 | 0 | -0.210819 | 0.77459667 | -0.1632993 | 0.163299316 | chmid |
| 9 | -1 | -1 | 1 | 0 | 1 | 1 | 0 | -0.421637 | 0.90369611 | -0.3810317 | 0.381031738 | 204.12 |
| 10 | 1 | 1 | 1 | 0 | -1 | 1 | 0 | 0.843274 | -0.3872983 | -0.3265986 | 0.326598632 | |
| 11 | -1 | 1 | 1 | 1 | 1 | 0 , | 0 | 0.6324555 | 0.77459667 | 0.48989795 | 0.489897949 | |
| 12 | 1 | -1 | 1 | 0 | 1 | 1 | 0 | -0.210819 | 0.90369611 | -0.1905159 | 0.190515869 | |
| 13 | -1 | -1 | 1 | 1 | -1 | 0 | 0 | -0.421637 | -0.5163978 | 0.21773242 | 0.217732422 | |
| 14 | 1 | 5 | 2 | | | | | | | | | |
| 15 | 15 TENSILE AXIS is above (input) | | | | | ove | (input) | | | | | |
| | | | | | | | this | | | | | ľ |
| | | | | | | | column | | | | | |
| | | | | | | | must be all | | | | | |
| 16 | | | | | | | zeros! | | | | | |
| | | | | | | | | | | | | |

You must submit a copy of the table of results showing how you calculated your answer which must display the maximum Schmid factor and the Miller indices of the activated slip system.

Q2. [30 points] *Compute Slip Matrices; verify 385 non-singular cases out of 792* Referring to slides 40 through 52 and #47 in particular, construct all the 5x5 slip matrices and determine which ones are non-singular. Verify that out of the ${}_5C_{12}$ combinations, only 384 are valid solutions, i.e. have a non-zero determinant. *Hints*:

Clearly you have to start by making a list of all 12 slip systems in fcc metals based on {111}<10>. Although this problem is deceptively simple, the main programming challenge is to compute a list of all the possible combinations of five slip systems (as opposed to just the number). Fortunately the web has code fragments that will do this (in C++, Fortran etc.), and Matlab has a built-in function.

What to submit:

You should submit your code (e.g. Matlab script).

- Q3. [40 points] *Bishop-Hill Model: Calculation of Taylor Factors for Multiple Slip* Assume that slip occurs on {111} planes and in <110> directions. For each of the three different strain types, uniaxial tension parallel to the Z axis, plane strain in the +X & -Z, and simple shear in the XZ sense (see the matrices below), calculate the following quantities.
- (a) the index of the active stress state (from the Bishop-Hill list);
- (b) the Taylor factor (to at least 2 decimal places) for crystals with the following orientations;
- (c) the active multi-slip stress state (as in the values of A, B, C, F, G, & H); for crystals with the following orientations.
- 2.1 (001)[100] 2.2 (0810)[100]
- 2.3 (-1 1 0) [1 1 1]
- 2.4 (213)[36-4]
- 2.5 (110)[-112].

The strain tensors for the 3 different strain types are as follows.

Uniaxial tension // Z:

$$\left[\begin{array}{cccc} -0.5 & 0 & 0 \\ 0 & -0.5 & 0 \\ 0 & 0 & 1 \end{array}\right]$$

Plane strain compression on +X and -Z:

$$\left[\begin{array}{ccc}
1 & 0 & 0 \\
0 & 0 & 0 \\
0 & 0 & -1
\end{array} \right]$$

Simple Shear on XZ:

| $\begin{bmatrix} 0 \end{bmatrix}$ | 0 | $1 \rceil$ |
|-----------------------------------|---|------------|
| 0 | 0 | 0 |
| 0 | 0 | 0 |

| Question | Orientation | Taylor Factor for Uniaxial Tension //Z | Stress State |
|----------|-------------------|--|-------------------------------|
| 2.1a | (0 0 1) [1 0 0] | 2.449 | 1.0, -1.0, 0.0, 0.0, 0.0, 0.0 |
| 2.2a | (0 8 10) [1 0 0] | 3.585 | 0.0, 0.0, 0.0, 1.0, 0.0, 0.0 |
| 2.3a | (-1 1 0) [1 1 1] | 3.674 | (to be determined by you) |

Answers are provided (above) for a few of the cases so that you can check your method. The meaning of the Miller indices is the conventional one discussed earlier in the class: (hkl) // sample-Z (=sample-3), [uvw] // sample-X (= sample-1).

The pseudo-code to obtain the Taylor factor is given in the lecture notes.

If you consider uniaxial tension for the three corners of the unit triangle (i.e. 001, 110 and 111), in which two corners is the inverse Schmid factor equal to the Taylor factor, and in which corner are they different?

Bishop & Hill stress states (Fortran style); factor of $\sqrt{6}$ *not* included:

```
stress(1,1)=1.
     stress(1,2)=-1.
     stress(1,3)=0.
     stress(1,4)=0.
     stress(1,5)=0.
     stress(1,6)=0.
# 1
     stress(2,1)=0.
     stress(2,2)=1.
     stress(2,3)=-1.
     stress(2,4)=0.
     stress(2,5)=0.
    stress(2,6)=0.
     stress(3,1)=-1.
     stress(3,2)=0.
     stress(3,3)=1.
     stress(3,4)=0.
```

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stress(3,5)=0.
      stress(3,6)=0.
! # 3
      stress(4,1)=0.
      stress(4,2)=0.
      stress(4,3)=0.
       stress(4,4)=1.
       stress(4,5)=0.
      stress(4,6)=0.
! # 4
      stress(5,1)=0.
      stress(5,2)=0.
      stress(5,3)=0.
      stress(5,4)=0.
      stress(5,5)=1.
      stress(5,6)=0.
! # 5
      stress(6,1)=0.
      stress(6,2)=0.
      stress(6,3)=0.
      stress(6,4)=0.
      stress(6,5)=0.
      stress(6,6)=1.
! # 6
      stress(7,1)=0.5
      stress(7,2)=-1.
      stress(7,3)=0.5
      stress(7,4)=0.
      stress(7,5)=0.5
      stress(7,6)=0.
! # 7
       stress(8,1)=0.5
       stress(8,2)=-1.
      stress(8,3)=0.5
      stress(8,4)=0.
      stress(8,5) = -0.5
      stress(8,6)=0.
! # 8
      stress(9,1)=-1.
       stress(9,2)=0.5
       stress(9,3)=0.5
       stress(9,4)=0.5
      stress(9,5)=0.
      stress(9,6)=0.
! # 9
       stress(10,1)=-1.
      stress(10,2)=0.5
      stress(10,3)=0.5
       stress(10,4)=-0.5
       stress(10,5)=0.
      stress(10,6)=0.
      stress(11,1)=0.5
       stress(11,2)=0.5
      stress(11,3)=-1.
      stress(11,4)=0.
       stress(11,5)=0.
      stress(11,6)=0.5
! # 11
      stress(12,1)=0.5
      stress(12,2)=0.5
      stress(12,3)=-1.
      stress(12,4)=0.
       stress(12,5)=0.
       stress(12,6) = -0.5
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```
stress(13,1)=0.5
stress(13,2)=0.
stress(13,3)=-0.5
stress(13,4)=0.5
stress(13,5)=0.
stress(13,6)=0.5
stress(14,1)=0.5
stress(14,2)=0.
stress(14,3) = -.5
stress(14,4)=-0.5
stress(14,5)=0.
stress(14,6)=0.5
stress(15,1)=0.5
stress(15,2)=0.
stress(15,3)=-0.5
stress(15,4)=0.5
stress(15,5)=0.
stress(15,6)=-0.5
stress(16,1)=0.5
stress(16,2)=0.
stress(16,3) = -0.5
stress(16,4)=-0.5
stress(16,5)=0.
stress(16,6)=-0.5
stress(17,1)=0.
stress(17,2)=-0.5
stress(17,3)=0.5
stress(17,4)=0.
stress(17,5)=0.5
stress(17,6)=0.5
stress(18,1)=0.
stress(18,2)=-0.5
stress(18,3)=0.5
stress(18,4)=0.
stress(18,5) = -0.5
stress(18,6)=0.5
stress(19,1)=0.
stress(19,2)=-0.5
stress(19,3)=0.5
stress(19,4)=0.
stress(19,5)=0.5
stress(19,6)=-0.5
stress(20,1)=0.
stress(20,2)=-0.5
stress(20,3)=0.5
stress(20,4)=0.
stress(20,5)=-0.5
stress(20,6)=-0.5
stress(21,1)=-0.5
stress(21,2)=0.5
stress(21,3)=0.
stress(21,4)=0.5
stress(21,5)=0.5
stress(21,6)=0.
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stress(22,1)=-0.5

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stress(22,2)=0.5
```

stress(22,3)=0.

stress(22,4)=-0.5

stress(22,5)=0.5 stress(22,6)=0.

stress(23,1)=-0.5

stress(23,2)=0.5

stress(23,3)=0.

stress(23,4)=0.5

stress(23,5)=-0.5stress(23,6)=0.

stress(24,1)=-0.5

stress(24,2)=0.5

stress(24,3)=0.

stress(24,4)=-0.5

stress(24,5)=-0.5

stress(24,6)=0.

stress(25,1)=0.

stress(25,2)=0.

stress(25,3)=0.

stress(25,4)=0.5stress(25,5)=0.5

stress(25,6) = -0.5

stress(26,1)=0.

stress(26,2)=0.

stress(26,3)=0.

stress(26,4)=0.5

stress(26,5)=-0.5

stress(26,6)=0.5

stress(27,1)=0.

stress(27,2)=0.

stress(27,3)=0.

stress(27,4)=-0.5

stress(27,5)=0.5

stress(27,6)=0.5

stress(28,1)=0.

stress(28,2)=0.

stress(28,3)=0. stress(28,4)=0.5

stress(28,5)=0.5

stress(28,6)=0.5